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X-ray source for generating monochromatic X-rays

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X-ray source for generating monochromatic X-rays

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The present invention relates to an X-ray source comprising an electron source for the emission of electrons, a target for the emission of X-rays in response to the incidence of the electrons and an outcoupling means for outcoupling of the X-rays. Further, the present invention relates to a target for use in such an X-ray source.

5 An X-ray source of this kind based on the production of bremsstrahlung radiation in a turbulently-flowing liquid metal, also called LIMAX (Liquid Metal Anode X-ray source), is described in US 6,185,277. The electrons enter the flowing liquid via an electron window which is a metal foil, for instance made of molybdenum or tungsten, or a diamond membrane. The electron window is sufficiently thin, in particular a few  $\mu\text{m}$ , so that  
10 the electron beam loses only a small portion of its initial energy in the window.

It is the object of the present invention to provide an X-ray source and a target for use in such an X-ray source which allows the generation of substantially monochromatic X-rays, by which a significant dose reduction can be achieved and which permits a higher power loadability compared to known X-ray sources.

15 This object is achieved according to the present invention by an X-ray source as claimed in claim 1 comprising:

- an electron source for the emission of electrons,
  - a target for the emission of characteristic, substantially monochromatic X-rays in response to the incidence of the electrons, said target comprising a metal foil of a thickness  
20 of less than  $10\mu\text{m}$  and a cooling circuit arranged to allow a coolant to flow along one side of said metal foil, wherein the metal of said metal foil has a high atomic number allowing the generation of X-rays and the coolant has a low atomic number not allowing the generation of X-rays, and
  - an outcoupling means for outcoupling of the X-rays on the side of the metal  
25 foil onto which the electrons are incident and which is opposite to the side of the coolant.
- A corresponding target for use in such an X-ray source is defined in claim 11.

The present invention is based on the idea to provide a discrete line X-ray source based on electron impact of a thin metal foil cooled by a flowing water beam dump. The basic idea is to discriminate against the bremsstrahlung radiation by observing the

radiation emitted on the side of the target onto which the electrons are incident, i. e. the radiation which is essentially antiparallel to the initial electron beam direction. The metal foil constituting the electron window is made sufficiently thin to preserve to a certain extent the angular collimation of the electron beam incident on the foil. The foil thickness is less than the electron diffusion depth; hence, a significant portion of the electron beam is deposited directly in the coolant. Whether this is a good assumption in a particular situation can only be ascertained by a simulation of the electron-photon transport, for instance a Monte-Carlo simulation. The power loadability of the proposed X-ray source is thus much greater than that of known stationary anode X-ray sources.

To aid optimization of the design parameters of the known LIMAX arrangement, a simple approach has been taken to determine the maximum focus temperature in dependence on such parameters of the liquid metal as the electron range, its diffusivity, flow velocity and degree of turbulence. The diffusion model yields results which are in relatively good agreement with those of a finite element program.

In the course of varying the input parameters to the above diffusion model the unexpected result was obtained that the thermal transport in a water-cooled arrangement leads to a factor of 10 increase in power loadability at constant focus temperature relative to the best liquid metal candidate. In quantitative terms, a focus of dimensions 1mm x 10mm could be loaded with an electron beam power of several tens of kW without exceeding the boiling point of water. This is exploited in the proposed X-ray source to obtain the high power loadability of the metal foil target by using a coolant having a low atomic number avoiding the generation of X-rays therein.

Preferred embodiments of the invention are defined in the dependent claims. While the invention generally works with a metal foil having a thickness of less than 10 $\mu$ m, the best results are obtained if the metal foil has a thickness of less than 5 $\mu$ m, preferably between 1 and 3 $\mu$ m. Furthermore, the metal foil is generally made of a metal which allows the generation of X-rays in response to the incidence of electrons. Preferred materials have an atomic number between 40 and 80. Good candidate materials are for instance tungsten, molybdenum or gold.

While generally the coolant has a low atomic number preventing the generation of X-rays in response to the incidence of electrons, the atomic number is preferably less than 10. Such liquids include water as well as oils based or hydrocarbon compounds. A high power loadability of the X-ray source has been obtained by using water as coolant.

To achieve a high flow velocity of the coolant at the area of the metal foil, a cooling circuit in which the coolant is flowing comprises a constriction at this area. Thus, a good cooling of the metal foil can be obtained and boiling of the coolant is prevented.

According to another preferred embodiment the target comprises a carrier supporting the metal foil on the side facing the coolant. Due to the very low thickness of the metal foil, depending on the material of the metal foil, it can be necessary to support it in order to increase mechanical stability. In this case an appropriate carrier, for instance a thin diamond layer, can be provided.

To avoid including bremsstrahlung radiation in the X-ray beam an outcoupling means, such as an X-ray window transparent to X-rays, is provided which generally only transmits X-rays propagating in the reflection direction of the metal foil, i.e. no X-rays in the transmission direction are outcoupled. In a preferred embodiment the outcoupling means only transmits X-rays propagating in a certain angular range from the reflection direction as defined in claim 8. This ensures that almost only characteristic monochromatic X-rays are outcoupled since bremsstrahlung radiation almost completely propagates in the transmission direction but not in the reflection direction and also not in said angular range.

According to another preferred embodiment the electrons are directed onto the surface of the metal foil at an angle of substantially  $90^\circ$ , i. e. perpendicular to the surface. In this direction the highest efficiency of producing X-rays can be ensured. However, to avoid the outcoupled X-ray beam obstructed by the electron source, the electron source is preferably located outside the X-ray beam, i. e. at an angle different from  $90^\circ$  to the surface of the metal foil. To ensure that the electrons hit the metal foil at an angle of substantially  $90^\circ$  appropriate means for directing the electron beam, for instance appropriate deflection coils, are provided.

The present invention will now be explained in more detail with reference to the drawings in which

Fig. 1 shows the photon spectrum of a thick target of a known X-ray tube,

Fig. 2 shows a polar plot of X-ray radiation from a thin W target,

Fig. 3 shows an embodiment of an X-ray source according to the present invention and

Fig. 4 shows a photon spectrum of a thin target according to the present invention.

Fig. 1 shows the photon spectrum from a known X-ray tube having a target with a massive W anode in response to an 150 keV electron beam using a 2mm Al filter and a 10° anode angle. The ratio of photons in the almost discrete K lines to the total number of photons in the spectrum is a measure for the monochromaticity  $M$  of the X-ray source. For the benefit of comparison with the X-ray source of the present invention the value of  $M$  for the spectrum shown in Fig. 1 is about 10 %. It is well known that electron diffusion makes a non-negligible contribution to the thermal transport in X-ray tube anodes. This contribution increases in solid-state, e. g. rotating anode X-ray tubes the shorter the time that the heat pulse has to diffuse through the target medium. The electron diffusion component can dominate the thermal transport when the anode has a relatively low conductivity. This is the case in a liquid anode tube when the anode consists of a coolant having a low atomic number rather than a liquid metal having a high atomic number. Very high values of loadability, i. e. power loading per unit area of focus leading to unit temperature rise in the anode (loadability having a unit of  $\text{W mm}^{-2} \text{K}^{-1}$ ) can be achieved by this. A loadability for a liquid water anode of  $50 \text{ W mm}^{-2} \text{K}^{-1}$  is feasible, and this is significantly higher than the maximum obtainable loadability with the known liquid metal anodes.

It is also established that the angular distribution of bremsstrahlung radiation is highly anisotropic for relativistic electron beams, with a marked preference for X-ray emission in the forwards direction. This situation is illustrated in Fig. 2 showing a polar plot of bremsstrahlung intensity  $B$  for 128 keV electrons on free W atoms. The atom is assumed to be at the centre of the plot and the electron beam propagates vertically upwards as indicated by the arrow  $E$ . The intensity is proportional to the vector length from the centre to the curve. The angular distribution of characteristic radiation  $C$  is also shown. As can be seen the angular distribution is isotropic, i. e. the intensity of characteristic radiation is substantially equal in all directions including the direction antiparallel to the direction of the electron beam  $E$ . The cross sections for photon production are differential in photon energy and emission angle.

These considerations together have led to the idea of a discrete line X-ray source based on electron impact on a thin metal foil cooled by a flowing coolant beam dump, where the coolant is particularly water. An embodiment of an X-ray source according to the present invention is shown in Fig. 3. An electron source, for instance a cathode, emits an electron beam  $E$  which under the influence of an external magnetic field generated by coils 2

rotates to enter the electron window 3 of the target 4 vertically. The electron window 3 comprises a thin metal foil 5 of a material whose K lines are to be excited supported if necessary by a thin carrier 6 of e. g. diamond.

5 The target 4 further comprises a cooling circuit 7 which can be a hollow tube in which a coolant 8 flows in the direction of the arrow 9. In order to increase the flow velocity of the coolant 8 in the area at the electron window 3, in particular under the metal foil 5, the cooling circuit 7 comprises a constriction 10 at this area, i.e. the cross section of the cooling circuit 7 is reduced compared to the cross section in other areas.

10 The thickness of the metal foil 5 is smaller than or equal to the electron diffusion depth which is the depth at which the energy loss per unit length projected onto the incidence direction of the electron beam E has its maximum value. It can be estimated from empirical formulae, or, better derived from Monte-Carlo programs for the electron transport. For 150 keV electrons incident on W foils its value is approximately  $4\mu\text{m}$ . Selecting the thickness of the metal foil smaller than or equal to the electron diffusion depth ensures that  
15 the electron velocity vectors will not have had opportunity to become isotropically distributed in direction.

The range of electrons of this energy is in tungsten approximately  $20\mu\text{m}$  from which it is evident that a significant proportion of the total electron energy will be deposited directly in the coolant. To a first approximation, the volume of coolant bombarded by  
20 electrons per second is  $V R L$ , where  $V$  is the flow speed of the coolant 8 in the constriction 10,  $L$  is the length of the electron focus perpendicular to the plane of the drawing of Fig. 3 and  $R$  is the electron range in water which is preferably selected as coolant. Hence the amount of energy this volume of water can take up per second for temperature rise  $\Delta T$  is  $V R L \Delta T C_p$  where the last factor is the heat capacity of water ( $4.2 \text{ MJ m}^{-3} \text{ K}^{-1}$ ). It has been  
25 assumed that the energy loss per unit length projected onto the incidence direction of the electron beam E is constant over the electron range. Inserting the values  $V = 50 \text{ m s}^{-1}$ ,  $R = 250\mu\text{m}$ ,  $L = 10^{-2} \text{ m}$ ,  $\Delta T = 25^\circ$  leads to a power of approximately 10 kW.

On the basis of the condition described above a foil thickness of less than  $5\mu\text{m}$ , preferably between 1 and  $3\mu\text{m}$ , for instance  $2\mu\text{m}$  is assumed. Approximately 5 % of the  
30 total power (about 1 kW) will be deposited in the foil 5. A temperature rise of  $\Delta T = 50^\circ$  is sufficient to remove this heat load with a water flow speed given above.

As the assumed coolant has a low mean atomic number  $Z$  and the cross section for production of bremsstrahlung is proportional to  $Z$  there will be comparatively little X-ray production in the coolant.

The electrons penetrating through the foil 5 interact either by collisional excitation to ionize the foil material or more occasionally through production of bremsstrahlung. The former involves the K shell electrons if the incoming electron has sufficient energy. The excited atom returns to its ground state by the emission of characteristic radiation e. g. with energy ( $K_{\alpha 1}$  line) of 57 keV. Characteristic radiation is emitted isotropically. The latter effect, bremsstrahlung radiation, is emitted almost completely in the transmission direction, i. e. in the downwards direction in Fig. 3, while the intensity of bremsstrahlung emission in the reflection direction, i. e. in the upwards direction in Fig. 3, particularly in the direction perpendicular to the surface of the metal foil 5, is very low.

Hence, if the foil emission is observed in the reflection direction, in particular over an angular range  $\alpha$  of, preferably  $\pm 20^\circ$  antiparallel to the electron beam direction, by use of appropriate outcoupling means 11, e.g. a window transparent to X-rays, it will be composed of a background of low intensity bremsstrahlung from the coolant 8 on which the characteristic lines of the metal of the foil 5 are superimposed. This results in a quasi-monochromatic spectrum of high radiance C. Monochromatic radiation is useful in a number of areas of medical and scientific radiology including, but not limited to investigations with reduced patient dose, calibration of detectors and development of new diagnostic modalities.

The mean energy loss by the electron beam E in the foil is approximately given by the Thomson-Whiddington-law which is itself derived from the Bethe-Bloch energy loss relationship. The Thomson-Whiddington-law is:  $E^2 = E_0^2 - xb \rho$ .  $E_0$  is the initial electron energy and x is the foil thickness in the initial direction of the electron beam required to reduce the mean electron energy to E. The other symbols have their customer meanings.

The Thomson-Whiddington constant b has a value for tungsten of  $8 \cdot 10^4 \text{ keV}^2 \text{ m}^2 \text{ kg}^{-1}$  at 150 keV. This results in an energy loss per  $\mu\text{m}$  foil thickness of 5 keV for thicknesses smaller compared with the electron range. The electron range is the value of foil thickness x required to reduce E to zero and is approximately  $20 \mu\text{m}$  from this equation.

A simulation result of the back-directed X-rays from the embodiment of the X-ray source shown in Fig. 3 having a  $2 \mu\text{m}$  thick W foil irradiated with 150 keV electrons is presented in Fig. 4. The spectrum shows the radiation emitted in a cone of opening semiangle  $15^\circ$  in a direction antiparallel to the initial electron beam direction. The monochromaticity parameter M defined above has a value of 0.45 for this arrangement and can be improved further by optimizing the geometry, high voltage and filtering.



## CLAIMS:

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1. An X-ray source comprising:
  - an electron source for the emission of electrons,
  - a target for the emission of characteristic, substantially monochromatic X-rays in response to the incidence of the electrons, said target comprising a metal foil of a thickness of less than  $10\mu\text{m}$  and a cooling circuit arranged to allow a coolant to flow along one side of said metal foil, wherein the metal of said metal foil has a high atomic number allowing the generation of X-rays and the coolant has a low atomic number not allowing the generation of X-rays, and
  - an outcoupling means for outcoupling of the X-rays on the side of the metal foil onto which the electrons are incident and which is opposite to the side of the coolant.
2. An X-ray source as claimed in claim 1, wherein the metal foil has a thickness of less than  $5\mu\text{m}$ , preferably between 1 and  $3\mu\text{m}$ .
3. An X-ray source as claimed in claim 1, wherein the metal of said metal foil has an atomic number between 40 and 80.
4. An X-ray source as claimed in claim 1, wherein the coolant has a mean atomic number of less than 10.
5. An X-ray source as claimed in claim 1, wherein the coolant is water.
6. An X-ray source as claimed in claim 1, wherein said cooling circuit comprises a constriction at the area of the metal foil.
7. An X-ray source as claimed in claim 1, wherein said target further comprises a carrier of low atomic number material, in particular having a mean atomic number of less than 10, supporting the metal foil on the side facing the coolant.

8. An X-ray source as claimed in claim 1, wherein said outcoupling means is adapted to outcouple X-rays at angles of an angular range from substantially 45° to 135°, in particular 70° to 110°, to the surface of the metal foil.

5 9. An X-ray source as claimed in claim 1, wherein said electrons are directed onto the surface of said metal foil at an angle of substantially 90°.

10. An X-ray source as claimed in claim 1, wherein said electron source is located outside the X-ray beam to be outcoupled, said X-ray source further comprising means for  
10 directing the electron beam onto the metal foil.

11. A target for use in an X-ray source for the generation of characteristic, substantially monochromatic X-rays in response to the incidence of electrons, said target comprising a metal foil of a thickness of less than 10µm and a cooling circuit arranged to  
15 allow a coolant to flow along one side of said metal foil, wherein the metal of said metal foil has a high atomic number allowing the generation of X-rays and the coolant has a low atomic number not allowing the generation of X-rays.

## ABSTRACT:

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The present invention relates to an X-ray source comprising an electron source (1) for the emission of electrons (E), a target (4) for the emission of characteristic, substantially monochromatic X-rays (C) in response to the incidence of the electrons (E) and an outcoupling means (11) for outcoupling of the X-rays. To achieve characteristic, substantially monochromatic X-rays with a high power loadability electrons are incident on a metal foil of a thickness of less than 10µm and a cooling circuit (7) is arranged to allow a coolant (8) to flow along one side of the metal foil (5), wherein the metal of the metal foil (5) has a high atomic number allowing the generation of X-rays and the coolant (8) has a low atomic number not allowing the generation of X-rays. The outcoupling means are adapted for outcoupling only X-rays (C) on the side of the metal foil (5) onto which the electrons (E) are incident and which is opposite to the side of the coolant (8) since on this side almost no bremsstrahlung radiation is generated.

Fig. 3

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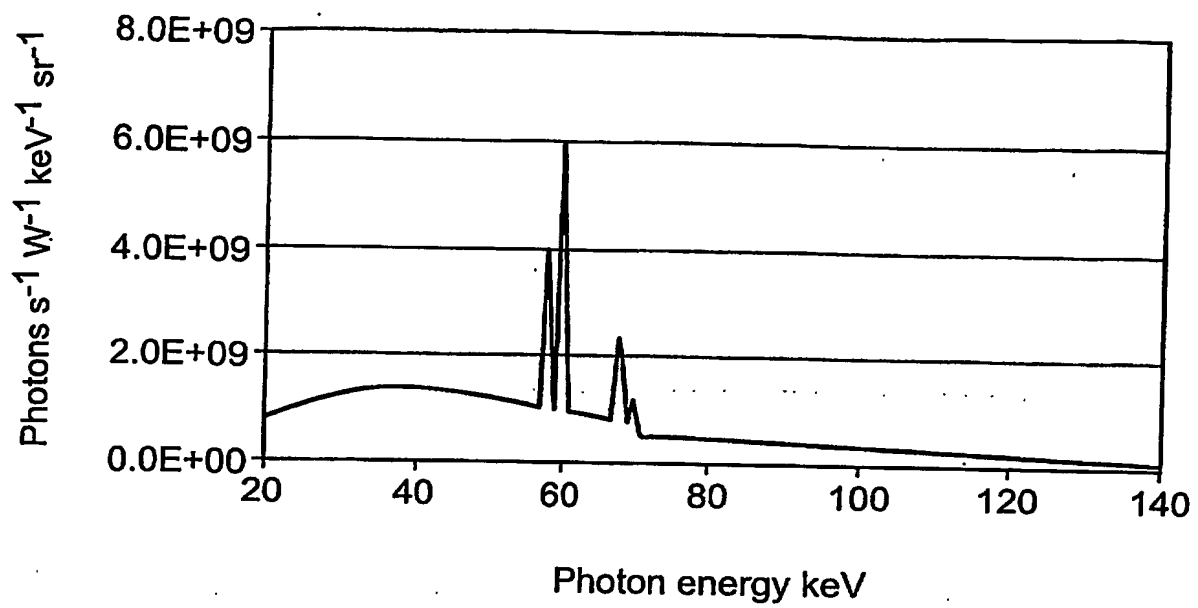


FIG.1

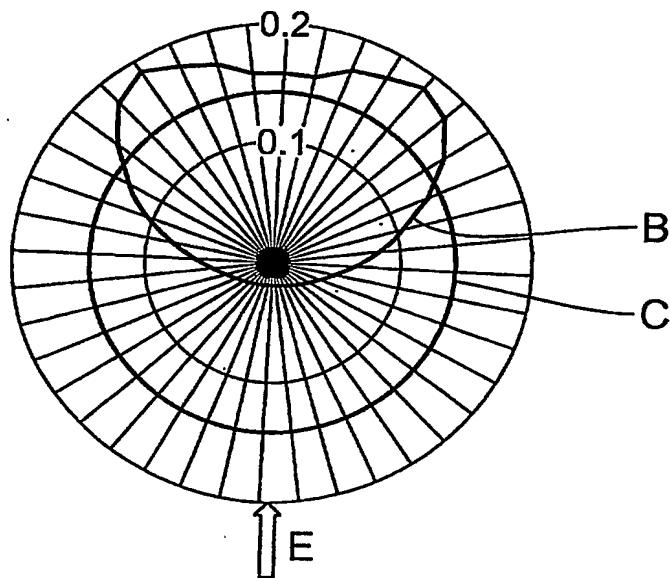


FIG.2

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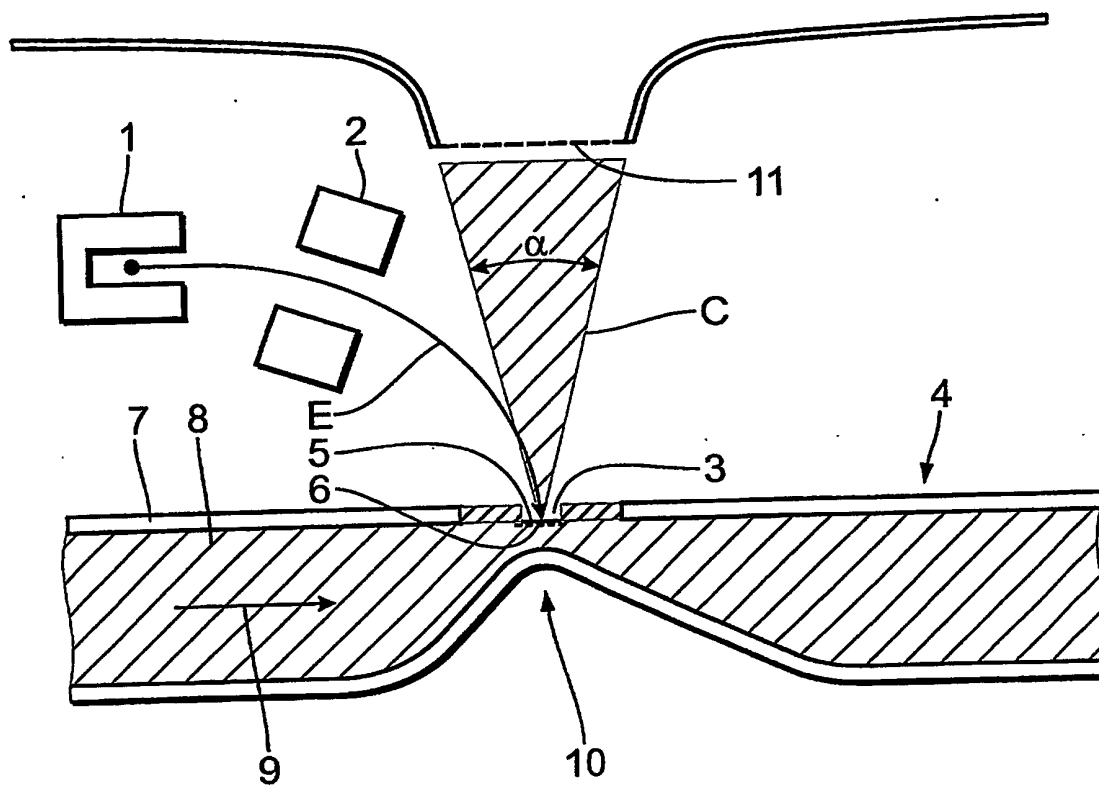


FIG.3

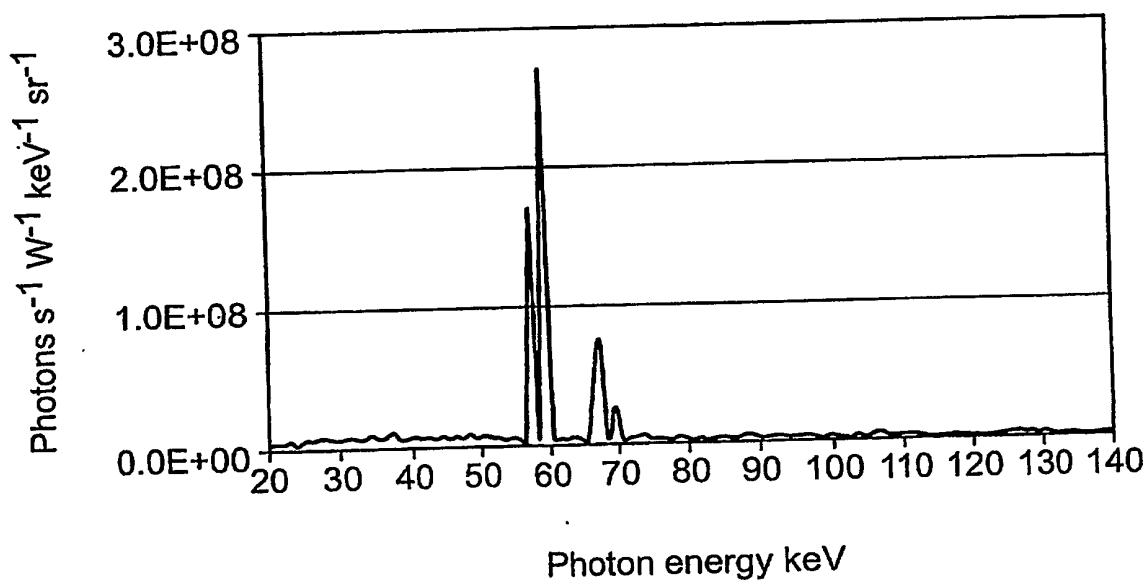


FIG.4

PCT Application

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